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| 1 | "Apparatus for Controlling Underwater Based |
|-----|--|
| . 2 | Equipment" |
| 3 | |
| 4 | Technical field |
| 5 | |
| 6 | The invention relates to an underwater location |
| 7 | device such as may be used for controlling the |
| 8 | launch, positioning or recovery of a tidal turbine |
| 9 | or other underwater equipment. It should be noted |
| 10 | that the example of a tidal turbine is used herein |
| 11 | but the invention is not limited to such uses. |
| 12 | |
| 13 | Background art |
| 14 | |
| 15 | Tidal currents offer a considerable source of |
| 16 | sustainable energy at various sites throughout the |
| 17 | world, usually within easy reach of land and in |
| 18 | relatively shallow waters. Tidal currents are |
| 19 | created by movement of the tides around the earth |
| 20 | producing a varying sea level, dependent on the . |
| 21 | phases of the moon and sun. As the sea levels vary |
| 22 | so the waters attempt to maintain equilibrium' |

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subject to gravitational forces, thus inducing flow 1 2 from one area of sea to another. This flow is modified by a number of factors such as, the 3 Coriolis forces due to the earth rotation, 4 5 earth/moon/sun alignment, local topography, atmospheric pressure and temperature and salinity 6 gradients. The major advantage of tidal power 7 8 generation is its regularity, which can be predicted 9 for years in advance. 10 According to a study by the ETSU (Energy Technology 11 12 Support Unit) the United Kingdom may obtain up to 20 13 percent of its total electricity by using these 14 systems to collect energy from fast moving tidal currents that exist in channels and offshore areas. 15 16 Similar resources have been noted to exist elsewhere 17 such as in the Straits of Messina, between Sicily 18 and mainland Italy. 19 20 The most powerful flows tend to occur in areas of 21 restriction, either by width or depth, but for the 22 same reasons are not suitable for widespread 23 exploitation by large, fixed devices which require a 24 minimum rotor area, and therefore water depth, to justify the costs of installation and maintenance. 25 It is assumed from the outset that new tidal barrage 26 27 systems are unlikely ever to be pursued due to their 28 inherent properties of high cost, delayed financial 29 return, and serious environmental consequences. 30 31 The considerable size of the available resource has 32 attracted various proposals for its exploitation.

3

The following represents the existing systems within 1 2 the field of tidal current energy extraction. assumed that power transmission problems will be 3 4 equal for any system, and that all systems will 5 require some form of non-toxic anti-fouling agent. 6 7 There also exist operational environmental impacts 8 common to all methods of tidal power generation, 9 such as, an inherent risk of collision damage to fish and marine mammals, redirection of currents and 10 the sediments and food particles contained within 11 them, and shipping, particularly fishing. 12 13 A first type of tidal current energy extraction 14 15 system encountered on the market is the Monopile This technology is well known and 16 system. understood by contractors familiar with the offshore 17 18 oil industry. It consists of twin axial flow turbines, each turbine driving a generator via a 19 20 gearbox, mounted on streamlined cantilevers either 21 side of a circular section, vertical steel monopile. 22 It is anticipated that a number of structures will 23 be grouped together in 'farms'. The planning of 24 such a tidal 'farm' would need to be accurately modelled for wake effects, as once installed, the 25 26 monopile is expensive to re-site. In addition, operational depth is restricted to the 20m - 35m 27 28 range. Concerning the installation and maintenance. monopile systems require a hole to be drilled in 29 suitable bedrock and the base of the turbine tower 30 31 is secured within the socket so produced. Existing 32 monopile support mechanisms for presenting a tidal

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turbine to the tidal currents are expensive, thus 1 making only a few sites economically viable for 2 power generation and requiring considerable sub sea 3 4 engineering expertise. 5 6 The current monopile systems permit raising the turbines above water level for maintenance and 7 8 repair, which is beneficial, but the long-term (i.e. 9 20 years) reliability and corrosion resistance of 10 the necessary mechanism must be questionable. protrusion of the piles above sea level would reduce 11 the likelihood of impact with passing vessels. 12 13 Concerning the environmental and decommissioning 14 15 issues, the impact of installation would be considerable, especially to the benthic flora and 16 fauna, but subsequently the piles may become areas 17 of shelter and therefore, populated. To minimise 18 19 the danger to shipping and fishing, decommissioning 20 would require complete removal of the piles, which 21 would disturb the benthic population once again. 22 A second type of tidal current energy extraction 23 system that exists in the prior art is the floating 24 25 tether. This floating tether device is anchored to 26 the seabed with a mooring cable and suspended clear 27 of the seabed using a flotation buoy. The axial 28 flow tidal current turbine is free to position 29 itself into the direction of the tidal flow, which 30 obviates the need for a yaw mechanism.

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Several prototypes have already been developed 1 2 including a 10-kilowatt device tested in Scotland in At present, the arrangement is unlikely to be 3 suitable for large power output installations due to 4 5 the relative sizes of anchor, turbine and float. 6 occasions of relatively high velocity tidal streams (e.g. spring tides), if the anchor holds, the 7 turbine will be dragged lower in the water with the 8 unwanted potential to collide with the seabed. 9 10 Concerning the installation of the floating tether 11 12 system, it is relatively quick and inexpensive. However, visual inspection would need to be frequent 13 14 as the structure is likely to be subject to storm damage and fatigue loading of the cable, leading to 15 possible loss of the supporting float and subsequent 16 sinking of the device, or loss of anchorage and 17 subsequent drifting. Once sunk, the device would be 18 19 open to damage by the oscillating tidal currents and 20 could prove difficult to recover, whilst a drifting 21 device would potentially cause damage to any other 22 moored turbines in its path. 23 24 Due to the length of tether required and the random 25 positioning of the device at any one time, this 26 arrangement is not suitable for closely grouped tidal farms and a safe spread would fail to make 27 economical use of the power available in a given 28 29 For the same reasons, this type of arrangement would present a hazard to all forms of 30 shipping, large and small. It would, however 31 32 present a possible solution to a one-off, small

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1 scale installation in areas such as the mouth of a 2 sea loch. Concerning the environmental impacts of installation and decommissioning of the floating 3 tether systems, it will be minimal, leaving no 4 5 footprint on removal. 6 7 A third type of tidal current energy extraction 8 system that also exists in the prior art is the oscillating hydroplane system. In that system, a 9 central post mounted on five legs supports a complex 10 mechanism comprising two interconnected symmetrical 11 12 hydrofoils. These hydrofoils are used to pump high-13 pressure oil, which drives an electrical generator via a hydraulic motor. At the end of each stroke, 14 the hydrofoils are tilted to give the required angle 15 of attack to produce the return stroke, thus 16 17 creating an oscillating motion. 18 19 Concerning the installation and maintenance, at present, the oscillating hydroplane system does not 20 21 yet possess a launch and recovery mechanism. 22 result of the constant oscillations and considerable number of moving parts, it is probable that this 23 device will be subject to high dynamic loading and 24 25 subsequent fatigue stress. The upward stroke of the 26 hydrofoils will tend to lift the device off the seabed and hence increase the possibility of it 27 being washed away at high tidal stream velocities. 28 29 30 Concerning the environmental impacts of installation and decommissioning of the oscillating hydroplane 31 32 systems, they are expected to be minimal, leaving no

| 1 | footprint on removal. However, this cannot be |
|-----------|--|
| 2 | confirmed until a launch/recovery mechanism is |
| 3 | proposed. Using high pressure oil as a means of |
| 4 | power transmission does however introduce the |
| 5 | possibility of pollution in the event of leakage. |
| 6 | |
| 7 | Some 'tidal' energy extraction systems can also be |
| 8 | used in freshwater applications such as rivers. |
| 9 | |
| 10 | With these existing systems and designs, it is a |
| L1 | problem that their instabilities during operations |
| 12 | as well as during launch and recovery, if possible, |
| 13 | might cause damage. In addition, since these |
| 14 | systems are becoming larger and larger, the frequent |
| L5 | installation and maintenance operations will become |
| L6 | more and more difficult and expensive. |
| L7 | · |
| L8 | Summary of the invention |
| L9 | |
| 20 | It is an object of the present invention to obviate |
| 21 | or mitigate the problems of controlling underwater |
| 22 | equipment in a flowstream. |
| 23 | · |
| 24 | In a first aspect, the invention described herein |
| 25 | relates to an apparatus for controlling underwater |
| 26 | equipment comprising: |
| 27 | attachment means for attaching underwater |
| 28 | equipment to the apparatus; and |
| 29 | at least one member for generating positive or |
| 30 | negative lift. |
| 31 | |

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Preferably, the at least one member is adapted to 1 2 create a negative lift due to fluid flow in a first direction and is adapted to create a negative lift 3 due to fluid flow in a second, different, direction. 4 5 Preferably, the first and second directions are 6 7 generally opposite to each other. 8 9 Preferably, the apparatus is adapted to anchor the underwater equipment to a sea- or river-bed. 10 11 12 Preferably, the attachment means is adapted to 13 attach the underwater equipment in close proximity 14 to the centre of gravity of the apparatus. 15 16 Preferably, the space frame is mounted on a number 17 of feet equipped with slippage prevention means, 18 which may be an arrangement of spikes or the like, to typically resist slipping by shear force rather 19 20 than relying on friction alone such that, in use, the negative lift will preferably tend to force said 21 22 slippage prevention means into a sea- or river-bed 23 thus resisting the drag forces acting on the space 24 frame tangentially to the seabed. 25 Preferably, the at least one member comprises at 26 27 least one hydrofoil. 28 29 Typically, differences in pressure acting on opposing surfaces of each of the at least one member 30 due to a predetermined angle of attack causes said 31

| 1 | at least one member to generate negative or positive |
|----|--|
| 2 | lift. |
| 3 | |
| 4 | Preferably, the apparatus is adapted to control the |
| 5 | launch and/or recovery of the underwater equipment |
| 6 | attached to it. |
| 7 | • |
| 8 | In a preferred embodiment, the at least one members |
| 9 | are rotatable to any position and even more |
| 10 | preferably in the region of 160° to 200° about a |
| 11 | longitudinal axis of the respective member. |
| 12 | |
| 13 | Preferably, the hydrofoils are symmetrical. |
| 14 | |
| 15 | Said at least one members preferably comprise at |
| 16 | least one hydrofoils which are more preferably self- |
| 17 | rectifying static hydrofoils, which may be capable |
| 18 | of passive rotation about an axis such that each |
| 19 | hydrofoil maintains alignment with a periodically |
| 20 | reciprocating rectilinear flow. |
| 21 | |
| 22 | Moreover, the at least one members are preferably |
| 23 | moveable between a first configuration in which they |
| 24 | are capable of generating positive lift and a second |
| 25 | configuration in which they are capable of |
| 26 | generating negative lift. |
| 27 | |
| 28 | Preferably, the at least one member has a variable |
| 29 | actuating means to vary the positive or negative |
| 30 | lift generated by the member. |
| 31 | |

| 1 | Preferably, said actuating means comprises a motor |
|-----|--|
| 2 | which may be a hydraulic, pneumatic or electric |
| 3 | actuated motor. Preferably, a shaft member is |
| 4 | actuated when a change between first and second |
| 5 | configurations is required, said actuation typically |
| 6 | causing the shaft member to rotate through a |
| 7 | predetermined angle, which may be in the region of |
| 8 | 180°. |
| . 9 | |
| 10 | Preferably, said apparatus comprises a support |
| 11 | framework which is typically composed of sub |
| 12 | frameworks, where a number of shaft members are |
| 13 | connected to the framework and on which said |
| 14 | symmetrical hydrofoils are coupled. Preferably, the |
| 15 | at least one hydrofoils are coupled to the support |
| 16 | framework by a respective bearing member connected |
| 17 | to the hydrofoil. The bearing member of the |
| 18 | hydrofoil is typically coupled to the shaft member |
| 19 | of the framework, the bearing member and shaft |
| 20 | member combining to provide a rotation enabling |
| 21 | portion and a rotation prevention portion. |
| 22 | Preferably, the bearing member is substantially |
| 23 | cylindrical. The rotation prevention portion |
| 24 | typically comprises at least one stop members (which |
| 25 | may be in the form of lugs mounted on the shaft |
| 26 | member) and which are adapted to engage with at |
| 27 | least one respective stop members (which may also be |
| 28 | lugs) mounted on the respective bearing member of |
| 29 | each hydrofoil. Typically, the bearing member |
| 30 | comprises a pair of stop members which are spaced |
| 31 | apart around its inner circumference, typically |
| 32 | being spaced apart by approximately 180°. |

| 1. | Typically, the shaft member comprises a pair of stop |
|------|--|
| 2 | members which are spaced apart around its outer |
| 3 | circumference, typically being spaced apart by |
| 4 | approximately 180°. Preferably, one of the bearing |
| 5 | stop members is engageable with a respective shaft |
| 6 | stop member to define the first negative |
| 7 | configuration and the other of the bearing stop |
| 8 | members is engageable with the other of the shaft |
| 9 | stop members to define the second negative |
| 10 | configuration. |
| 11 | |
| . 12 | Preferably, said apparatus is a multi-legged, self- |
| 13 | levelling space frame equipped with a plurality of |
| 14 | hydrofoils, typically at different heights. |
| 15 | |
| 16 | In alternative embodiments, the at least one member |
| 17 | is rigidly connected to a support framework and is |
| 18 | unsymmetrical. Preferably, the at least one member |
| 19 | comprises a disc shaped member which, in use, is |
| 20 | adapted to produce positive or negative lift |
| 21 | regardless of the direction of flow of fluid |
| 22 | thereby. Preferably, the disc shaped member |
| 23 | produces negative lift. |
| 24 | |
| 25 | According to a second aspect of the invention, there |
| 26 | is provided a method of controlling underwater |
| 27 | equipment; the method comprising: |
| 28 | providing an apparatus having at least one |
| 29 | member for generating positive or negative lift; |
| 30 | attaching the apparatus to underwater |
| 31 | equipment; |
| 32 | releasing the apparatus into a fluid; |

| 1 | allowing fluid to flow past the at least one |
|----|---|
| 2 | member to generate positive or negative lift. |
| 3 | |
| 4 | Preferably, the method according to the second |
| 5 | aspect of the invention is performed using the |
| 6 | apparatus according to the first aspect of the |
| 7 | invention. |
| 8 | |
| 9 | Preferably, the apparatus is placed in a flow of |
| 10 | water. |
| 11 | |
| 12 | Preferably, the underwater equipment is a turbine. |
| 13 | |
| 14 | According to a further aspect of the present |
| 15 | invention, there is provided an apparatus for |
| 16 | maintaining underwater equipment within a sea or |
| 17 | river tidal current location, the apparatus |
| 18 | comprising at least one moveable members capable of |
| 19 | generating negative lift, where said at least one |
| 20 | members are moveable between a first configuration |
| 21 | in which they create a negative lift due to flow in |
| 22 | a first direction, and a second configuration in |
| 23 | which they create a negative lift due to flow in a |
| 24 | second, different, direction. |
| 25 | |
| 26 | The invention also provides energy extracting |
| 27 | apparatus for extracting energy from fluid flow, |
| 28 | said energy extracting apparatus comprising: |
| 29 | a turbine; |
| 30 | at least one member, which in use, generates |
| 31 | positive or negative lift. |

| T | |
|----|--|
| 2 | Brief description of the drawings |
| 3 | |
| 4 | Embodiments of the present invention will now be |
| 5 | described, by way of example only, with reference to |
| 6 | the accompanying drawings, in which:- |
| 7 | |
| 8 | Figure 1 shows a side view of a space frame in |
| 9 | accordance with the present invention, showing |
| 10 | a tubular frame allowing the positioning of the |
| 11 | hydrofoils at differing heights; |
| 12 | Figures 2a to 2d show the passive reversing of |
| 13 | the hydrofoils in response to a change in flow |
| 14 | direction whilst Figures 2e to 2h show the |
| 15 | different movements of hydrofoils of Figure 1 |
| 16 | actuated by hydraulic motors to create positive |
| 17 | and negative lifts during launch, recovery and |
| 18 | transitional operations according to the |
| 19 | present invention; |
| 20 | Figures 2i to 2m show the passive reversing of |
| 21 | the hydrofoils in response to a change in flow |
| 22 | direction; |
| 23 | Figure 3 in its upper half shows a first side |
| 24 | view, and in its lower half shows an opposite |
| 25 | side view, illustrating the fundamental |
| 26 | geometry of the passive reversing mechanism; |
| 27 | Figure 3a in its upper half shows a first side |
| 28 | view, and in its lower half shows an opposite |
| 29 | side view, illustrating the fundamental |
| 30 | geometry of the passive reversing mechanism; |

| 1 | Figure 3b is a third side view showing the |
|----|--|
| 2 | fundamental geometry of the passive reversing |
| 3 | mechanism; |
| 4 | Figure 4 shows in detail the assemblage of |
| 5 | hydrofoils onto the space frame of Figure 1; |
| 6 | Fig. 5a is a side view of a second embodiment |
| 7 | of an apparatus in accordance with the present |
| 8 | invention and an attached canister; |
| 9 | Fig. 5b is a front view of the Fig. 5a |
| 10 | apparatus with the attached canister; |
| 11 | Fig. 5c is a plan view of the Fig. 5a apparatus |
| 12 | with the attached canister; and, |
| 13 | Figs. 5d-5f are a series of views of an |
| 14 | attachment ring which forms part of the Fig. 5a |
| 15 | apparatus. |
| 16 | |
| 17 | Detailed description of the invention |
| 18 | |
| 19 | According to the present invention, the apparatus |
| 20 | for launching an underwater device from a vessel, |
| 21 | securing the underwater device whilst in operation |
| 22 | on the seabed and permitting recovery to a vessel, |
| 23 | for maintenance and repair should be as simple as |
| 24 | possible without involving any sophisticated and |
| 25 | specialised equipment. A first embodiment of the |
| 26 | invention is shown in Figure 1 and utilises passive, |
| 27 | self-rectifying static hydrofoils, the central shaft |
| 28 | (see Figure 3) of which can be rotated through 180° |
| 29 | to generate positive or negative lift as required. |
| 30 | |
| 31 | As is shown in Figure 1, the apparatus 1 for |
| 32 | controlling the launch, secure positioning and |

| 1 | recovery of an underwater device comprises a space |
|----|--|
| 2 | frame 10 for attaching to any desired underwater |
| 3 | device such as power extraction equipment which may |
| 4 | comprise a tidal turbine (not shown), a hydrofoil |
| 5 | support frame to accommodate the self rectifying |
| 6 | hydrofoil mechanisms 12 and hydraulically operated |
| 7 | legs 11 for levelling of the apparatus 1. The feet |
| 8 | 14 are equipped with spikes or similar serrated |
| 9 | attachments (not shown) to initiate grip on the sea |
| 10 | or river bed. |
| 11 | |
| 12 | The hydrofoils 12 are inclined in such a way as to |
| 13 | generate a significant downforce as a result of the |
| 14 | stream flow over their surfaces. This downforce |
| 15 | will push the apparatus 1 into the seabed, and, |
| 16 | since the actual applied force will be proportional |
| 17 | to the square of the velocity of the fluid passing |
| 18 | over them, the apparatus 1 will be more securely |
| 19 | fixed as the streamflow velocity increases. By this |
| 20 | means the apparatus can overcome overturning moments |
| 21 | applied to the underwater device that it supports. |
| 22 | |
| 23 | The space frame 10 is shown as arched tubing but is |
| 24 | not restricted to shape since any frame |
| 25 | configuration offering different levels of mounting |
| 26 | point for the hydrofoils 12 will suffice. The |
| 27 | apparatus 1 as shown has multiple hydrofoils 12 but |
| 28 | any number of hydrofoils 12 will suffice. As is |
| 29 | shown in Figures 2a to 2h, each hydrofoil 12 is |
| 30 | mounted on a central shaft 48 such that it may |
| 31 | rotate upwards from horizontal (or any angle of |
| 32 | inclination above horizontal) through vertical to |
| | |

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any angle above horizontal but now pointing in the opposite direction. The angle of attack of the

3 hydrofoils 12 is governed by the relative size and

4 positioning of lugs 46 attached to the central shaft

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5 48 and the corresponding lobes 44 attached to an

outer shaft (not shown) which is itself fixed to the

7 hydrofoil 12.

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9 In a preferred embodiment, the apparatus 1 according

10 to the present invention comprises a multi-legged,

11 self-levelling space frame 10 equipped with a number

of hydrofoils 12 at different heights with any

underwater device, such as a tidal turbine, it

14 supports, situated as close as practicable to the

15 centre of gravity of the apparatus 1.

16

17 It is anticipated that the space frame 10 will be

18 mounted on a number of feet 14 equipped with spikes

19 (not shown) to resist slipping of the apparatus 1

20 with respect to the river bed (not shown) by shear

21 force rather than relying on friction alone. The

22 number of feet 14A, 14B required will depend on the

23 weight of the apparatus 1; however, the location and

24 the shape of these supporting feet 14A, 14B aim at

25 holding the apparatus 1 in the orientation shown in

26 Figure 1 upwards against the current and thus

ensuring the stability of the space frame 10. The

28 negative lift (arrow A) will tend to force these

29 spikes into the sea or river bed (not shown in

30 Figure 1) thus resisting the drag forces acting on

31 the space frame 10 tangentially to the sea or river

32 bed.

| 1 | |
|----|--|
| 2 | The drag forces acting on the underwater device |
| 3 | (such as the tidal turbine) attached to the |
| 4 | apparatus 1 will naturally tend to apply an |
| 5 | overturning moment to the space frame 10 about its |
| 6 | rearmost feet 14B, with respect to the direction of |
| 7 | flow (arrow F). These forces will however be |
| 8 | overcome by positioning the hydrofoils 12 at |
| 9 | stations such that the negative lift (arrow A), |
| 10 | created by the foremost or upstream (those at the |
| 11 | left hand side of the space frame 10 as shown in |
| 12 | Figure 1) hydrofoils 12 acting over the length of |
| 13 | the space frame 10, is arranged to exceed the |
| 14 | overturning moment. |
| 15 | |
| 16 | Thus, the space frame 10 is symmetrical about its |
| 17 | midpoint M with the hydrofoils 12 being coupled to |
| 18 | the space frame 10 in a manner, to be subsequently |
| 19 | detailed in a discussion of Figures 2a to 2h, which |
| 20 | allows them to passively reverse with stream flow F |
| 21 | to maintain compressive forces in a downwards |
| 22 | direction A and restraining moments regardless of |
| 23 | tidal stream direction. |
| 24 | |
| 25 | During operation of the apparatus 1, the hydrofoils |
| 26 | 12 are free to rotate (shown as clockwise in Figures |
| 27 | 2a to 2d and 2I to 2m) in response to the change in |
| 28 | tidal stream flow F direction in a manner which is |
| 29 | shown from left to right in Figures 2a to 2d to |
| 30 | create a negative lift (arrow A) so as to push the |
| 31 | apparatus 1 into the seabed. |

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When the apparatus 1 is to be installed on the seabed or is to be recovered from the seabed for

e.g. maintenance of the apparatus 1, as shown in the

4 Figures 2a to 2d, hydraulic motors 30, via a

5 suitable gearing mechanism such as a worm and wheel

6 arrangement 32 (as shown in Figure 3) or chain type

7 mechanism (not shown), are utilised to rotate (shown

8 as anticlockwise in Figures 2e to 2h) the

9 longitudinal axes (i.e. the horizontal axes

10 perpendicular to the stream flow 12) of the

11 hydrofoils 12 through the required angle until the

12 hydrofoils 12 have reached the configuration shown

13 Figure 2h; for the configuration shown in Figures 2e

14 to 2h, this angle is approximately 180°. It should

be kept in mind that the hydraulic motors 30 can be

16 replaced by pneumatic or electric motors. In other

words, if the apparatus 1 is towed, e.g. by a boat

or other vessel or installation at the surface, the

19 hydrofoils 12 will produce positive lift (arrow B)

as shown in Figures 2e to 2h. For launch and

21 recovery, this positive lift can be utilised to

22 raise or lower the space frame 10 within the tidal

23 stream. If required, this action could be augmented

24 by forming air tanks within the space frame 10 that

25 can be 'blown' with compressed air to improve the

buoyancy of the apparatus 1. If the hydraulic

27 motors 30 use the worm and wheel mechanism 32 form

28 of drive, the hydrofoil 12 positions can be altered

over a range of positions, thus permitting the

30 apparatus 1 to be 'flown' in the water. Hydraulic

31 connections (and pneumatic connections if required)

19

can be affixed to a supporting marker buoy (not 1 2 shown) for ease of access. 3 4 Figure 3 shows the mechanism and assemblage of hydrofoils 12, hydraulic motors 30 and worm and 5 wheel drive shaft mechanisms 32 in more detail. 6 The 7 hydrofoils 12 are free to rotate about a central 8 shaft 48, through an included angle of say 160° 9 which will maintain an angle of 10° to the 10 horizontal. The 10° angle effectively becomes an 11 angle of attack when the tidal stream flow F 12 Thus as the tidal stream 10 reciprocates, the hydrofoils 12 will maintain an angle of 10°, 13 creating a negative lift (arrow A), which will 14 therefore push the spikes 16 into the seabed and 15 16 immobilise the space frame 10. As will be described 17 subsequently, positioning lugs 46 mounted on a central shaft 48 provided a stop for locating lobes 18 19 44 of the hydrofoil 12, such that the hydrofoil 12 cannot rotate further than the 160° shown in Figures 20 21 2a to 2d. 22 23 By rotating the central shaft 48 through slightly greater than 180° (say 200°), the negative lift 24 becomes positive lift (arrow B) and the space frame 25 26 10 will rise through the water so that the tidal 27 turbine 90 can be recovered on the vessel (not 28 shown). 29 Figure 4 shows in more detail the mechanical 30 assemblage of hydrofoils 12 with space frame 10. 31 32 The hydraulic motor 30 for actuating the positioning

20

gear is equipped with a drive shaft 32 that is 1 utilised for rotating an indented positioning gear 2 42 or a toothed gear wheel. The positioning gear 42 3 is solidly attached to a central shaft 48 which 4 passes through a bore provided in the larger end of 5 each hydrofoil 12, a section of which is show on 6 Figure 4. The bore of the hydrofoil 12 is provided 7 with a pair of diametrically opposed and inwardly 8 projecting hydrofoil locating lobes 44. The central 9 shaft 48 has a pair of diametrically opposed and 10 outwardly projecting positioning lugs 46, each one 11 of which selectively co-operates with one of the 12 13 respective pair of diametrically opposed hydrofoil 14 locating lobes 44. 15 Thus, by rotating the drive shaft 32, the hydraulic 16 motor 30 actuates or rotates the position gear 42 17 18 which in turn rotates the central shaft 48. positioning lugs 46 will contact the locating lobes 19 44 and carry them 44 (and the hydrofoil 12) about 20 the rotational axis of the central shaft 48 until 21 the hydrofoil 12 is in the desired configuration, 22 this being through an angle of approximately 160° 23 until the hydrofoil 12 is in the configuration shown 24 in Figure 2h. At this point, the motor 30 is de-25 actuated and the positioning lugs 46 will hold the 26 27 hydrofoil 12 locked in this configuration. rotation of 160° enables the hydrofoil 12 to 28 29 maintain an angle of 10° to the horizontal in order to provide an angle of attack when the tidal stream 30 31 F reverses. 32

21

Conversely, the rotation of the central shaft 48 by 1 2 180° drives the hydrofoils 12 to create a positive lift and in which case, the space frame 10 will rise 3 through water. Figure 3a shows how the attitude of 4 5 the hydrofoil 12 is changed by a simple 180° clockwise rotation of the central shaft 48. 6 7 8 The apparatus according to the present invention, 9 can be launched and recovered by a non-specialist 10 vessel, using non-specialist equipment. Indeed if the vessel is large enough, a number of apparatus 1 11 may be launched or recovered in a day without the 12 need to return to port. This will also permit easy 13 14 access for maintenance and repair. Since apparatus 15 1 possesses few moving parts and no complex mechanisms, it should be inherently reliable. 16 17 A second embodiment of an apparatus in accordance 18 with the present invention is shown in Figs. 5a-5d. 19 20 The apparatus 100 comprises a tripod support frame 21 110, a bottom ring or stand 126, a disc-shaped 22 hydrofoil 112, support brackets 120 and an 23 attachment ring 122 with bolts 123. The apparatus 24 100 is attached to an ADCP canister 124 via the 25 attachment ring 122 and bolts 123. Other subsea 26 equipment may also be attached to the apparatus 100 27 in place of the canister 124. 28 29 The hydrofoil 112 is rigidly connected to the frame 30 110 via the support brackets 120 and its plane is 31 generally parallel to the main plane defined by the 32 bottom ring 126 such that the hydrofoil 122 will be

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generally parallel to the seabed in use. A central 1 2 aperture 119 is provided within the hydrofoil 112. A lower face 113 of the hydrofoil 112 faces the 3 stand 126 and is of a generally flat surface, 4 whereas its opposite, upper, face 115 faces away 5 6 from the stand 126 and gradually curves upwards away from the main plane of the hydrofoil as it 7 approaches the central aperture 119 to form a raised 8 lip portion 117. This can be achieved by the 9 10 assembly of a plurality of smaller hydrofoils 112s to produce a multi-faceted hydrofoil 112. 11 12 hydrofoil 112 thus has rotational symmetry around a central axis 118 but is not symmetrical on either 13 14 side of its main plane. 15 16 Thus when a flow of water passes over each face 113, 115 of the hydrofoil 112, the reaction force of the 17 18 water on the raised lip 117 pushes the hydrofoil 112 19 along with the other components of the apparatus 100 20 and ADCP canister 124 in a downwards direction -21 that is "negative lift" results. 22 23 Thus in use, the hydrofoil helps to direct the apparatus 100 and attached equipment towards the 24 25 seabed and once in position, the hydrofoil maintains the apparatus and equipment on the seabed. 26 27 28 The apparatus 100 may be attached to a line (not shown) and the line attached at its other end to a 29 If the apparatus needs to be recovered, the 30 buoy. 31 apparatus may be pulled in by the line.

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An advantage of certain embodiments of the present 1 invention, such as the second embodiment, is that 2 they continue to perform their function of providing 3 negative lift regardless of the direction of flow of 4 5 the water. 6 7 An advantage of the second embodiment of the invention is that it includes no moving parts and so 8 is reliable and requires minimal maintenance. 9 10 The embodiments described herein may also be 11 provided with an integral turbine or other 12 underwater equipment rather than attaching such 13 equipment to the apparatus before use. 14 15 16 Although reference is made to employing the 17 apparatus 1, 100 in a tidal current and in certain 18 embodiments using a tidal turbine, it is to be 19 understood that the apparatus 1, 100 may be placed in any flow of liquid such as rivers and are not 20 21 limited to their use tidal areas. 22 23 An advantage of certain embodiments of the present invention is that they permit the launch and 24 25 recovery of underwater equipment to be carried out using a non-specialist but suitably equipped vessel. 26 27 Concerning the primary environmental impact of 28 embodiments of apparatus 1 according to the present 29 invention, it would have some impact upon the 30 31 benthic flora and fauna, and, although the positioning and retrieval of apparatus 1 would be 32

| 1 | relatively frequent (at least once every year is |
|----|--|
| 2 | anticipated), nothing more than temporary localised |
| 3 | disturbance is anticipated. There exists some |
| 4 | potential for hydraulic oil leakage, but the system |
| 5 | contents are minimal so, even in the event of |
| 6 | complete system evacuation, any oil contamination |
| 7 | would be minor. Operational environmental hazards |
| 8 | are in common with the other forms of tidal energy |
| 9 | extraction and decommissioning would leave no |
| 10 | footprint. |
| 11 | |
| 12 | Improvements and modifications in terms of |
| 13 | dimensions and locations of the different parts |
| 14 | described above may be incorporated to the |
| 15 | hereinbefore described apparatus for controlling the |
| 16 | launch and recovery of a tidal turbine without |
| 17 | departing from the scope of the present invention. |